

REFERENCE: BP8.R019

PROJECT: N/A

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STATE OF NORTH CAROLINA
 DEPARTMENT OF TRANSPORTATION
 DIVISION OF HIGHWAYS
 GEOTECHNICAL ENGINEERING UNIT

STRUCTURE
SUBSURFACE INVESTIGATION

COUNTY RANDOLPH
 PROJECT DESCRIPTION BRIDGE NO. 162 ON LANES
MILL ROAD (SR 1005) OVER BRUSH CREEK

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	BP8.R019	1	30

CAUTION NOTICE

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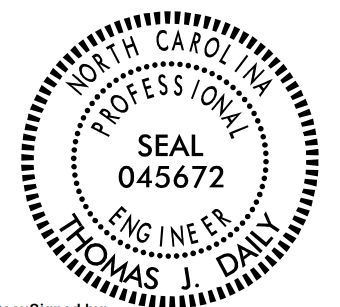
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SIGNATURE DATE

**DOCUMENT NOT CONSIDERED FINAL
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NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
 DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT
SUBSURFACE INVESTIGATION
 SOIL AND ROCK LEGEND, TERMS, SYMBOLS, AND ABBREVIATIONS

SOIL DESCRIPTION

SOIL IS CONSIDERED UNCONSOLIDATED, SEMI-CONSOLIDATED, OR WEATHERED EARTH MATERIALS THAT CAN BE PENETRATED WITH A CONTINUOUS FLIGHT POWER AUGER AND YIELD LESS THAN 100 BLOWS PER FOOT ACCORDING TO THE STANDARD PENETRATION TEST (AASHTO T 208, ASTM D1586). SOIL CLASSIFICATION IS BASED ON THE AASHTO SYSTEM. BASIC DESCRIPTIONS GENERALLY INCLUDE THE FOLLOWING: CONSISTENCY, COLOR, TEXTURE, MOISTURE, AASHTO CLASSIFICATION, AND OTHER PERTINENT FACTORS SUCH AS MINERALOGICAL COMPOSITION, ANGULARITY, STRUCTURE, PLASTICITY, ETC. FOR EXAMPLE, *VERY STIFF, GRAY, SILTY CLAY, MOIST WITH INTERBEDDED FINE SAND LAYERS, HIGHLY PLASTIC, A-7-6*

SOIL LEGEND AND AASHTO CLASSIFICATION

GENERAL CLASS.	GRANULAR MATERIALS (≤ 35% PASSING #200)							SILT-CLAY MATERIALS (> 35% PASSING #200)							ORGANIC MATERIALS					
	A-1	A-3	A-2	A-2-4	A-2-5	A-2-6	A-2-7	A-4	A-5	A-6	A-7	A-1, A-2	A-3	A-4, A-5	A-6, A-7					
GROUP CLASS.	A-1-a	A-1-b	A-2	A-2-4	A-2-5	A-2-6	A-2-7	A-4	A-5	A-6	A-7	A-1, A-2	A-3	A-4, A-5	A-6, A-7					
SYMBOL	[Pattern]							[Pattern]							[Pattern]					
% PASSING #10 #40 #200	50 MX 30 MX 15 MX	50 MX 25 MX	51 MN 35 MX	35 MX 35 MX	35 MX 35 MX	35 MX 35 MX	35 MX 35 MX	36 MN 36 MN	36 MN 36 MN	36 MN 36 MN	36 MN 36 MN	GRANULAR SOILS	SILT-CLAY SOILS	MUCK, PEAT						
MATERIAL PASSING #40 LL PI	[Values]							[Values]							[Values]					
GROUP INDEX	[Values]							[Values]							[Values]					
USUAL TYPES OF MAJOR MATERIALS	STONE FRAGS. GRAVEL, AND SAND			FINE SAND				SILTY OR CLAYEY GRAVEL AND SAND				SILTY SOILS		CLAYEY SOILS		SOILS WITH LITTLE OR MODERATE AMOUNTS OF ORGANIC MATTER				
GEN. RATING AS SUBGRADE	EXCELLENT TO GOOD							FAIR TO POOR							FAIR TO POOR	POOR	UNSUITABLE			

PI OF A-7-5 SUBGROUP IS ≤ LL - 30 ; PI OF A-7-6 SUBGROUP IS > LL - 30

CONSISTENCY OR DENSENESS

PRIMARY SOIL TYPE	COMPACTNESS OR CONSISTENCY	RANGE OF STANDARD PENETRATION RESISTANCE (N-VALUE)	RANGE OF UNCONFINED COMPRESSIVE STRENGTH (TONS/FT ²)
GENERALLY GRANULAR MATERIAL (NON-COHESIVE)	VERY LOOSE LOOSE MEDIUM DENSE DENSE VERY DENSE	< 4 4 TO 10 10 TO 30 30 TO 50 > 50	N/A
GENERALLY SILT-CLAY MATERIAL (COHESIVE)	VERY SOFT SOFT MEDIUM STIFF STIFF VERY STIFF HARD	< 2 2 TO 4 4 TO 8 8 TO 15 15 TO 30 > 30	< 0.25 0.25 TO 0.5 0.5 TO 1.0 1 TO 2 2 TO 4 > 4

TEXTURE OR GRAIN SIZE

U.S. STD. SIEVE SIZE OPENING (MM)	4	10	40	60	200	270
	4.76	2.00	0.42	0.25	0.075	0.053
BOULDER (BLDR.)						
COBBLE (COB.)						
GRAVEL (GR.)						
COARSE SAND (CSE, SD.)						
FINE SAND (F SD.)						
SILT (SL.)						
CLAY (CL.)						

SOIL MOISTURE - CORRELATION OF TERMS

SOIL MOISTURE SCALE (ATTERBERG LIMITS)	FIELD MOISTURE DESCRIPTION	GUIDE FOR FIELD MOISTURE DESCRIPTION
LL - LIQUID LIMIT	- SATURATED - (SAT.)	USUALLY LIQUID; VERY WET, USUALLY FROM BELOW THE GROUND WATER TABLE
PL - PLASTIC LIMIT	- WET - (W)	SEMISOLID; REQUIRES DRYING TO ATTAIN OPTIMUM MOISTURE
OM - OPTIMUM MOISTURE SHRINKAGE LIMIT	- MOIST - (M)	SOLID; AT OR NEAR OPTIMUM MOISTURE
SL - SHRINKAGE LIMIT	- DRY - (D)	REQUIRES ADDITIONAL WATER TO ATTAIN OPTIMUM MOISTURE

PLASTICITY

	PLASTICITY INDEX (PI)	DRY STRENGTH
NON PLASTIC	0-5	VERY LOW
SLIGHTLY PLASTIC	6-15	SLIGHT
MODERATELY PLASTIC	16-25	MEDIUM
HIGHLY PLASTIC	26 OR MORE	HIGH

COLOR

DESCRIPTIONS MAY INCLUDE COLOR OR COLOR COMBINATIONS (TAN, RED, YELLOW-BROWN, BLUE-GRAY). MODIFIERS SUCH AS LIGHT, DARK, STREAKED, ETC. ARE USED TO DESCRIBE APPEARANCE.

GRADATION

WELL GRADED - INDICATES A GOOD REPRESENTATION OF PARTICLE SIZES FROM FINE TO COARSE.
 UNIFORMLY GRADED - INDICATES THAT SOIL PARTICLES ARE ALL APPROXIMATELY THE SAME SIZE.
 GAP-GRADED - INDICATES A MIXTURE OF UNIFORM PARTICLE SIZES OF TWO OR MORE SIZES.

ANGULARITY OF GRAINS

THE ANGULARITY OR ROUNDNESS OF SOIL GRAINS IS DESIGNATED BY THE TERMS: ANGULAR, SUBANGULAR, SUBROUNDED, OR ROUNDED.

MINERALOGICAL COMPOSITION

MINERAL NAMES SUCH AS QUARTZ, FELDSPAR, MICA, TALC, KAOLIN, ETC. ARE USED IN DESCRIPTIONS WHEN THEY ARE CONSIDERED OF SIGNIFICANCE.

COMPRESSIBILITY

SLIGHTLY COMPRESSIBLE	LL < 31
MODERATELY COMPRESSIBLE	LL = 31 - 50
HIGHLY COMPRESSIBLE	LL > 50

PERCENTAGE OF MATERIAL

ORGANIC MATERIAL	GRANULAR SOILS	SILT - CLAY SOILS	OTHER MATERIAL
TRACE OF ORGANIC MATTER	2 - 3%	3 - 5%	TRACE 1 - 10%
LITTLE ORGANIC MATTER	3 - 5%	5 - 12%	LITTLE 10 - 20%
MODERATELY ORGANIC	5 - 10%	12 - 20%	SOME 20 - 35%
HIGHLY ORGANIC	> 10%	> 20%	HIGHLY 35% AND ABOVE

GROUND WATER

- Water level in bore hole immediately after drilling
- Static water level after 24 hours
- Perched water, saturated zone, or water bearing strata
- Spring or seep

MISCELLANEOUS SYMBOLS

- Roadway embankment (RE) with soil description
- Soil symbol
- Artificial fill (AF) other than roadway embankment
- Inferred soil boundary
- Inferred rock line
- Alluvial soil boundary
- DIP & DIP DIRECTION OF ROCK STRUCTURES
- TEST BORING
- AUGER BORING
- CORE BORING
- MONITORING WELL
- PIEZOMETER INSTALLATION
- SLOPE INDICATOR INSTALLATION
- CONE PENETROMETER TEST
- SOUNDING ROD
- TEST BORING WITH CORE
- SPT N-VALUE

RECOMMENDATION SYMBOLS

- UNDERCUT
- SHALLOW UNDERCUT
- UNCLASSIFIED EXCAVATION - UNSUITABLE WASTE
- UNCLASSIFIED EXCAVATION - ACCEPTABLE DEGRADABLE ROCK
- UNCLASSIFIED EXCAVATION - ACCEPTABLE, BUT NOT TO BE USED IN THE TOP 3 FEET OF EMBANKMENT OR BACKFILL

ABBREVIATIONS

- AR - AUGER REFUSAL
- BT - BORING TERMINATED
- CL - CLAY
- CPT - CONE PENETRATION TEST
- CSE - COARSE
- DMT - DILATOMETER TEST
- DPT - DYNAMIC PENETRATION TEST
- e - VOID RATIO
- F - FINE
- FOSS. - FOSSILIFEROUS
- FRAC. - FRACTURED, FRACTURES
- FRAGS. - FRAGMENTS
- HL - HIGHLY
- MED. - MEDIUM
- MICA - MICACEOUS
- MOD. - MODERATELY
- NP - NON PLASTIC
- ORG. - ORGANIC
- PMT - PRESSUREMETER TEST
- SAP. - SAPROLITE
- SD. - SAND, SANDY
- SL. - SILT, SILTY
- SLI. - SLIGHTLY
- TCR - TRICONE REFUSAL
- w - MOISTURE CONTENT
- V - VERY
- VST - VANE SHEAR TEST
- WEA. - WEATHERED
- UNIT WEIGHT
- DRY UNIT WEIGHT
- SAMPLE ABBREVIATIONS
- S - BULK
- SS - SPLIT SPOON
- ST - SHELBY TUBE
- RS - ROCK
- RT - RECOMPACTED TRIAXIAL
- CBR - CALIFORNIA BEARING RATIO

EQUIPMENT USED ON SUBJECT PROJECT

- DRILL UNITS:
 - CME-45C
 - CME-55
 - CME-550
 - VANE SHEAR TEST
 - PORTABLE HOIST
 - D-50
- ADVANCING TOOLS:
 - CLAY BITS
 - 6" CONTINUOUS FLIGHT AUGER
 - 8" HOLLOW AUGERS
 - HARD FACED FINGER BITS
 - TUNG-CARBIDE INSERTS
 - CASING w/ ADVANCER
 - TRICONE *STEEL TEETH
 - TRICONE *TUNG-CARB.
 - CORE BIT
- HAMMER TYPE:
 - AUTOMATIC
 - MANUAL
- CORE SIZE:
 - B
 - H
 - N Q
- HAND TOOLS:
 - POST HOLE DIGGER
 - HAND AUGER
 - SOUNDING ROD
 - VANE SHEAR TEST

ROCK DESCRIPTION

HARD ROCK IS NON-COASTAL PLAIN MATERIAL THAT WOULD YIELD SPT REFUSAL IF TESTED, AN INFERRED ROCK LINE INDICATES THE LEVEL AT WHICH NON-COASTAL PLAIN MATERIAL WOULD YIELD SPT REFUSAL, SPT REFUSAL IS PENETRATION BY A SPLIT SPOON SAMPLER EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS IN NON-COASTAL PLAIN MATERIAL. THE TRANSITION BETWEEN SOIL AND ROCK IS OFTEN REPRESENTED BY A ZONE OF WEATHERED ROCK. ROCK MATERIALS ARE TYPICALLY DIVIDED AS FOLLOWS:

- WEATHERED ROCK (WR)
- CRYSTALLINE ROCK (CR)
- NON-CRYSTALLINE ROCK (NCR)
- COASTAL PLAIN SEDIMENTARY ROCK (CP)

WEATHERING

- FRESH: ROCK FRESH, CRYSTALS BRIGHT, FEW JOINTS MAY SHOW SLIGHT STAINING. ROCK RINGS UNDER HAMMER IF CRYSTALLINE.
- VERY SLIGHT (V SLI): ROCK GENERALLY FRESH, JOINTS STAINED, SOME JOINTS MAY SHOW THIN CLAY COATINGS IF OPEN, CRYSTALS ON A BROKEN SPECIMEN FACE SHINE BRIGHTLY. ROCK RINGS UNDER HAMMER BLOWS IF OF A CRYSTALLINE NATURE.
- SLIGHT (SLI): ROCK GENERALLY FRESH, JOINTS STAINED AND DISCOLORATION EXTENDS INTO ROCK UP TO 1 INCH. OPEN JOINTS MAY CONTAIN CLAY. IN GRANITOID ROCKS SOME OCCASIONAL FELDSPAR CRYSTALS ARE DULL AND DISCOLORED. CRYSTALLINE ROCKS RING UNDER HAMMER BLOWS.
- MODERATE (MOD): SIGNIFICANT PORTIONS OF ROCK SHOW DISCOLORATION AND WEATHERING EFFECTS. IN GRANITOID ROCKS, MOST FELDSPARS ARE DULL AND DISCOLORED, SOME SHOW CLAY. ROCK HAS DULL SOUND UNDER HAMMER BLOWS AND SHOWS SIGNIFICANT LOSS OF STRENGTH AS COMPARED WITH FRESH ROCK.
- MODERATELY SEVERE (MOD. SEV.): ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. IN GRANITOID ROCKS, ALL FELDSPARS DULL AND DISCOLORED AND A MAJORITY SHOW KAOLINIZATION. ROCK SHOWS SEVERE LOSS OF STRENGTH AND CAN BE EXCAVATED WITH A GEOLOGIST'S PICK. ROCK GIVES "CLUNK" SOUND WHEN STRUCK. *IF TESTED, WOULD YIELD SPT REFUSAL*
- SEVERE (SEV.): ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC CLEAR AND EVIDENT BUT REDUCED IN STRENGTH TO STRONG SOIL. IN GRANITOID ROCKS ALL FELDSPARS ARE KAOLINIZED TO SOME EXTENT. SOME FRAGMENTS OF STRONG ROCK USUALLY REMAIN. *IF TESTED, WOULD YIELD SPT N VALUES > 100 BPF*
- VERY SEVERE (V SEV.): ALL ROCK EXCEPT QUARTZ DISCOLORED OR STAINED. ROCK FABRIC ELEMENTS ARE DISCERNIBLE BUT MASS IS EFFECTIVELY REDUCED TO SOIL STATUS, WITH ONLY FRAGMENTS OF STRONG ROCK REMAINING. SAPROLITE IS AN EXAMPLE OF ROCK WEATHERED TO A DEGREE THAT ONLY MINOR VESTIGES OF ORIGINAL ROCK FABRIC REMAIN. *IF TESTED, WOULD YIELD SPT N VALUES < 100 BPF*
- COMPLETE: ROCK REDUCED TO SOIL. ROCK FABRIC NOT DISCERNIBLE, OR DISCERNIBLE ONLY IN SMALL AND SCATTERED CONCENTRATIONS. QUARTZ MAY BE PRESENT AS DIKES OR STRINGERS. SAPROLITE IS ALSO AN EXAMPLE.

ROCK HARDNESS

- VERY HARD: CANNOT BE SCRATCHED BY KNIFE OR SHARP PICK. BREAKING OF HAND SPECIMENS REQUIRES SEVERAL HARD BLOWS OF THE GEOLOGIST'S PICK.
- HARD: CAN BE SCRATCHED BY KNIFE OR PICK ONLY WITH DIFFICULTY. HARD HAMMER BLOWS REQUIRED TO DETACH HAND SPECIMEN.
- MODERATELY HARD: CAN BE SCRATCHED BY KNIFE OR PICK. GOUGES OR GROOVES TO 0.25 INCHES DEEP CAN BE EXCAVATED BY HARD BLOW OF A GEOLOGIST'S PICK. HAND SPECIMENS CAN BE DETACHED BY MODERATE BLOWS.
- MEDIUM HARD: CAN BE GROOVED OR GOUGED 0.05 INCHES DEEP BY FIRM PRESSURE OF KNIFE OR PICK POINT. CAN BE EXCAVATED IN SMALL CHIPS TO PIECES 1 INCH MAXIMUM SIZE BY HARD BLOWS OF THE POINT OF A GEOLOGIST'S PICK.
- SOFT: CAN BE GROOVED OR GOUGED READILY BY KNIFE OR PICK. CAN BE EXCAVATED IN FRAGMENTS FROM CHIPS TO SEVERAL INCHES IN SIZE BY MODERATE BLOWS OF A PICK POINT. SMALL, THIN PIECES CAN BE BROKEN BY FINGER PRESSURE.
- VERY SOFT: CAN BE CARVED WITH KNIFE. CAN BE EXCAVATED READILY WITH POINT OF PICK. PIECES 1 INCH OR MORE IN THICKNESS CAN BE BROKEN BY FINGER PRESSURE. CAN BE SCRATCHED READILY BY FINGER NAIL.

FRACTURE SPACING

TERM	SPACING	TERM	THICKNESS
VERY WIDE	MORE THAN 10 FEET	VERY THICKLY BEDDED	4 FEET
WIDE	3 TO 10 FEET	THICKLY BEDDED	1.5 - 4 FEET
MODERATELY CLOSE	1 TO 3 FEET	THINLY BEDDED	0.16 - 1.5 FEET
CLOSE	0.16 TO 1 FOOT	VERY THINLY BEDDED	0.03 - 0.16 FEET
VERY CLOSE	LESS THAN 0.16 FEET	THICKLY LAMINATED	0.008 - 0.03 FEET
		THINLY LAMINATED	< 0.008 FEET

INDURATION

- FOR SEDIMENTARY ROCKS, INDURATION IS THE HARDENING OF MATERIAL BY CEMENTING, HEAT, PRESSURE, ETC.
- FRIABLE: RUBBING WITH FINGER FREES NUMEROUS GRAINS; GENTLE BLOW BY HAMMER DISINTEGRATES SAMPLE.
- MODERATELY INDURATED: GRAINS CAN BE SEPARATED FROM SAMPLE WITH STEEL PROBE; BREAKS EASILY WHEN HIT WITH HAMMER.
- INDURATED: GRAINS ARE DIFFICULT TO SEPARATE WITH STEEL PROBE; DIFFICULT TO BREAK WITH HAMMER.
- EXTREMELY INDURATED: SHARP HAMMER BLOWS REQUIRED TO BREAK SAMPLE; SAMPLE BREAKS ACROSS GRAINS.

TERMS AND DEFINITIONS

- ALLUVIUM (ALLUV.): SOILS THAT HAVE BEEN TRANSPORTED BY WATER.
- AQUIFER - A WATER BEARING FORMATION OR STRATA.
- ARENACEOUS - APPLIED TO ROCKS THAT HAVE BEEN DERIVED FROM SAND OR THAT CONTAIN SAND.
- ARGILLACEOUS - APPLIED TO ALL ROCKS OR SUBSTANCES COMPOSED OF CLAY MINERALS, OR HAVING A NOTABLE PROPORTION OF CLAY IN THEIR COMPOSITION, SUCH AS SHALE, SLATE, ETC.
- ARTESIAN - GROUND WATER THAT IS UNDER SUFFICIENT PRESSURE TO RISE ABOVE THE LEVEL AT WHICH IT IS ENCOUNTERED, BUT WHICH DOES NOT NECESSARILY RISE TO OR ABOVE THE GROUND SURFACE.
- CALCAREOUS (CALC.): SOILS THAT CONTAIN APPRECIABLE AMOUNTS OF CALCIUM CARBONATE.
- COLLUVIUM - ROCK FRAGMENTS MIXED WITH SOIL DEPOSITED BY GRAVITY ON SLOPE OR AT BOTTOM OF SLOPE.
- CORE RECOVERY (REC.) - TOTAL LENGTH OF ALL MATERIAL RECOVERED IN THE CORE BARREL DIVIDED BY TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
- DIKE - A TABULAR BODY OF IGNEOUS ROCK THAT CUTS ACROSS THE STRUCTURE OF ADJACENT ROCKS OR CUTS MASSIVE ROCK.
- DIP - THE ANGLE AT WHICH A STRATUM OR ANY PLANAR FEATURE IS INCLINED FROM THE HORIZONTAL.
- DIP DIRECTION (DIP AZIMUTH) - THE DIRECTION OR BEARING OF THE HORIZONTAL TRACE OF THE LINE OF DIP, MEASURED CLOCKWISE FROM NORTH.
- FAULT - A FRACTURE OR FRACTURE ZONE ALONG WHICH THERE HAS BEEN DISPLACEMENT OF THE SIDES RELATIVE TO ONE ANOTHER PARALLEL TO THE FRACTURE.
- FISSILE - A PROPERTY OF SPLITTING ALONG CLOSELY SPACED PARALLEL PLANES.
- FLOAT - ROCK FRAGMENTS ON SURFACE NEAR THEIR ORIGINAL POSITION AND DISLODGED FROM PARENT MATERIAL.
- FLOOD PLAIN (FP) - LAND BORDERING A STREAM, BUILT OF SEDIMENTS DEPOSITED BY THE STREAM.
- FORMATION (FM) - A MAPPABLE GEOLOGIC UNIT THAT CAN BE RECOGNIZED AND TRACED IN THE FIELD.
- JOINT - FRACTURE IN ROCK ALONG WHICH NO APPRECIABLE MOVEMENT HAS OCCURRED.
- LEDGE - A SHELF-LIKE RIDGE OR PROJECTION OF ROCK WHOSE THICKNESS IS SMALL COMPARED TO ITS LATERAL EXTENT.
- LENS - A BODY OF SOIL OR ROCK THAT THINS OUT IN ONE OR MORE DIRECTIONS.
- MOTTLED (MOT.) - IRREGULARLY MARKED WITH SPOTS OF DIFFERENT COLORS. MOTTLING IN SOILS USUALLY INDICATES POOR AERATION AND LACK OF GOOD DRAINAGE.
- PERCHED WATER - WATER MAINTAINED ABOVE THE NORMAL GROUND WATER LEVEL BY THE PRESENCE OF AN INTERVENING IMPERVIOUS STRATUM.
- RESIDUAL (RES.) SOIL - SOIL FORMED IN PLACE BY THE WEATHERING OF ROCK.
- ROCK QUALITY DESIGNATION (RQD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF CORE RUN AND EXPRESSED AS A PERCENTAGE.
- SAPROLITE (SAP.) - RESIDUAL SOIL THAT RETAINS THE RELIC STRUCTURE OR FABRIC OF THE PARENT ROCK.
- SILL - AN INTRUSIVE BODY OF IGNEOUS ROCK OF APPROXIMATELY UNIFORM THICKNESS AND RELATIVELY THIN COMPARED WITH ITS LATERAL EXTENT, THAT HAS BEEN EMPLACED PARALLEL TO THE BEDDING OR SCHISTOSITY OF THE INTRUDED ROCKS.
- SLICKENSIDE - POLISHED AND STRIATED SURFACE THAT RESULTS FROM FRICTION ALONG A FAULT OR SLIP PLANE.
- STANDARD PENETRATION TEST (PENETRATION RESISTANCE) (SPT) - NUMBER OF BLOWS (N OR BPF) OF A 140 LB. HAMMER FALLING 30 INCHES REQUIRED TO PRODUCE A PENETRATION OF 1 FOOT INTO SOIL WITH A 2 INCH OUTSIDE DIAMETER SPLIT SPOON SAMPLER. SPT REFUSAL IS PENETRATION EQUAL TO OR LESS THAN 0.1 FOOT PER 60 BLOWS.
- STRATA CORE RECOVERY (SCRC) - TOTAL LENGTH OF STRATA MATERIAL RECOVERED DIVIDED BY TOTAL LENGTH OF STRATUM AND EXPRESSED AS A PERCENTAGE.
- STRATA ROCK QUALITY DESIGNATION (SROD) - A MEASURE OF ROCK QUALITY DESCRIBED BY TOTAL LENGTH OF ROCK SEGMENTS WITHIN A STRATUM EQUAL TO OR GREATER THAN 4 INCHES DIVIDED BY THE TOTAL LENGTH OF STRATA AND EXPRESSED AS A PERCENTAGE.
- TOPSOIL (TS) - SURFACE SOILS USUALLY CONTAINING ORGANIC MATTER.

BENCH MARK: BM2 N: 688961 E: 1828888

ELEVATION: 446.21 FEET

NOTES:

FIAD: FILLED IMMEDIATELY AFTER DRILLING

NORTH CAROLINA DEPARTMENT OF TRANSPORTATION
DIVISION OF HIGHWAYS
GEOTECHNICAL ENGINEERING UNIT

SUBSURFACE INVESTIGATION

SUPPLEMENTAL LEGEND, GEOLOGICAL STRENGTH INDEX (GSI) TABLES
FROM AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS

AASHTO LRFD Figure 10.4.6.4-1 — Determination of GSI for Jointed Rock Mass (Marinos and Hoek, 2000)

AASHTO LRFD Figure 10.4.6.4-2 — Determination of GSI for Tectonically Deformed Heterogeneous Rock Masses (Marinos and Hoek, 2000)

GEOLOGICAL STRENGTH INDEX (GSI) FOR JOINTED ROCKS (Hoek and Marinos, 2000)		SURFACE CONDITIONS					GSI FOR HETEROGENEOUS ROCK MASSES SUCH AS FLYSCH (Marinos, P and Hoek E., 2000)		SURFACE CONDITIONS OF DISCONTINUITIES (Predominantly bedding planes)										
<p>From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. Note that the table does not apply to structurally controlled failures. Where weak planar structural planes are present in an unfavorable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.</p>		VERY GOOD	GOOD	FAIR	POOR	VERY POOR	<p>From a description of the lithology, structure and surface conditions (particularly of the bedding planes), choose a box in the chart. Locate the position in the box that corresponds to the condition of the discontinuities and estimate the average value of GSI from the contours. Do not attempt to be too precise. Quoting a range from 33 to 37 is more realistic than giving GSI = 35. Note that the Hoek-Brown criterion does not apply to structurally controlled failures. Where unfavourably oriented continuous weak planar discontinuities are present, these will dominate the behaviour of the rock mass. The strength of some rock masses is reduced by the presence of groundwater and this can be allowed for by a slight shift to the right in the columns for fair, poor and very poor conditions. Water pressure does not change the value of GSI and it is dealt with by using effective stress analysis.</p>	VERY GOOD	GOOD	FAIR	POOR	VERY POOR							
		Very rough, fresh unweathered surfaces	Rough, slightly weathered, iron stained surfaces	Smooth, moderately weathered and altered surfaces	Slickensided, highly weathered surfaces with compact coatings or fillings or angular fragments	Slickensided, highly weathered surfaces with soft clay coatings or fillings		Very Rough, fresh unweathered surfaces	Rough, slightly weathered surfaces	Smooth, moderately weathered and altered surfaces	Very smooth, occasionally slickensided surfaces with compact coatings or fillings with angular fragments	Very smooth, slickensided or highly weathered surfaces with soft clay coatings or fillings							
STRUCTURE		DECREASING SURFACE QUALITY →					COMPOSITION AND STRUCTURE												
<p>INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities</p> <p>BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets</p> <p>VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets</p> <p>BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity</p> <p>DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces</p> <p>LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes</p>	<p>DECREASING INTERLOCKING OF ROCK PIECES</p>	90	80	70	60	50	40	30	20	10	N/A	N/A	70	60	50	40	30	20	10
									<p>A. Thick bedded, very blocky sandstone. The effect of pelitic coatings on the bedding planes is minimized by the confinement of the rock mass. In shallow tunnels or slopes these bedding planes may cause structurally controlled instability.</p>										
									<p>B. Sandstone with thin inter-layers of siltstone</p> <p>C. Sandstone and siltstone in similar amounts</p> <p>D. Siltstone or silty shale with sandstone layers</p> <p>E. Weak siltstone or clayey shale with sandstone layers</p>										
									<p>C, D, E, and G - may be more or less folded than illustrated but this does not change the strength. Tectonic deformation, faulting and loss of continuity moves these categories to F and H.</p>										
									<p>F. Tectonically deformed, intensively folded/faulted, sheared clayey shale or siltstone with broken and deformed sandstone layers forming an almost chaotic structure</p>										
									<p>G. Undisturbed silty or clayey shale with or without a few very thin sandstone layers</p> <p>H. Tectonically deformed silty or clayey shale forming a chaotic structure with pockets of clay. Thin layers of sandstone are transformed into small rock pieces.</p>										
							<p>→ Means deformation after tectonic disturbance</p>												

09/26/22

PROJECT: BP8.R019

CONTRACT:

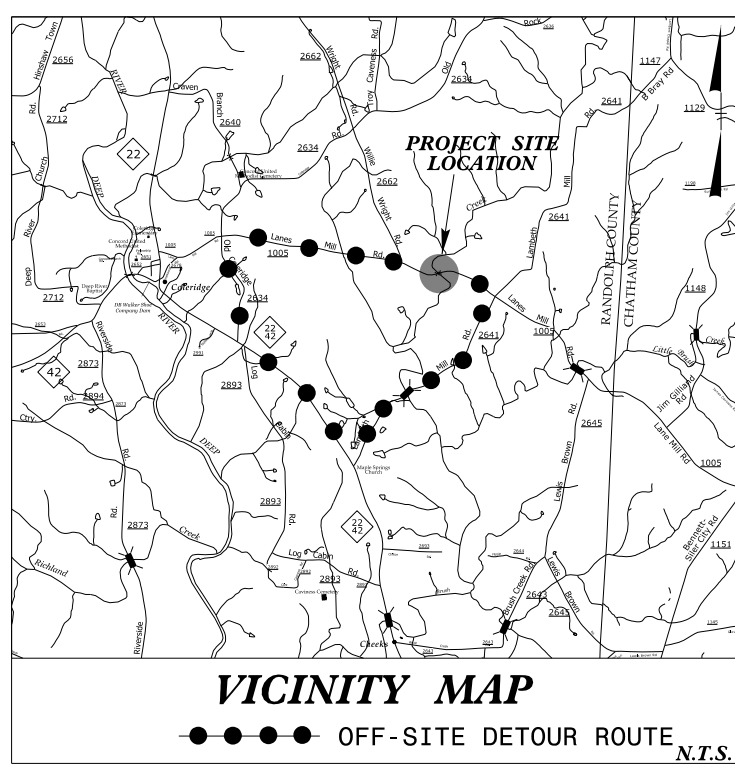
STATE OF NORTH CAROLINA
DIVISION OF HIGHWAYS

RANDOLPH COUNTY

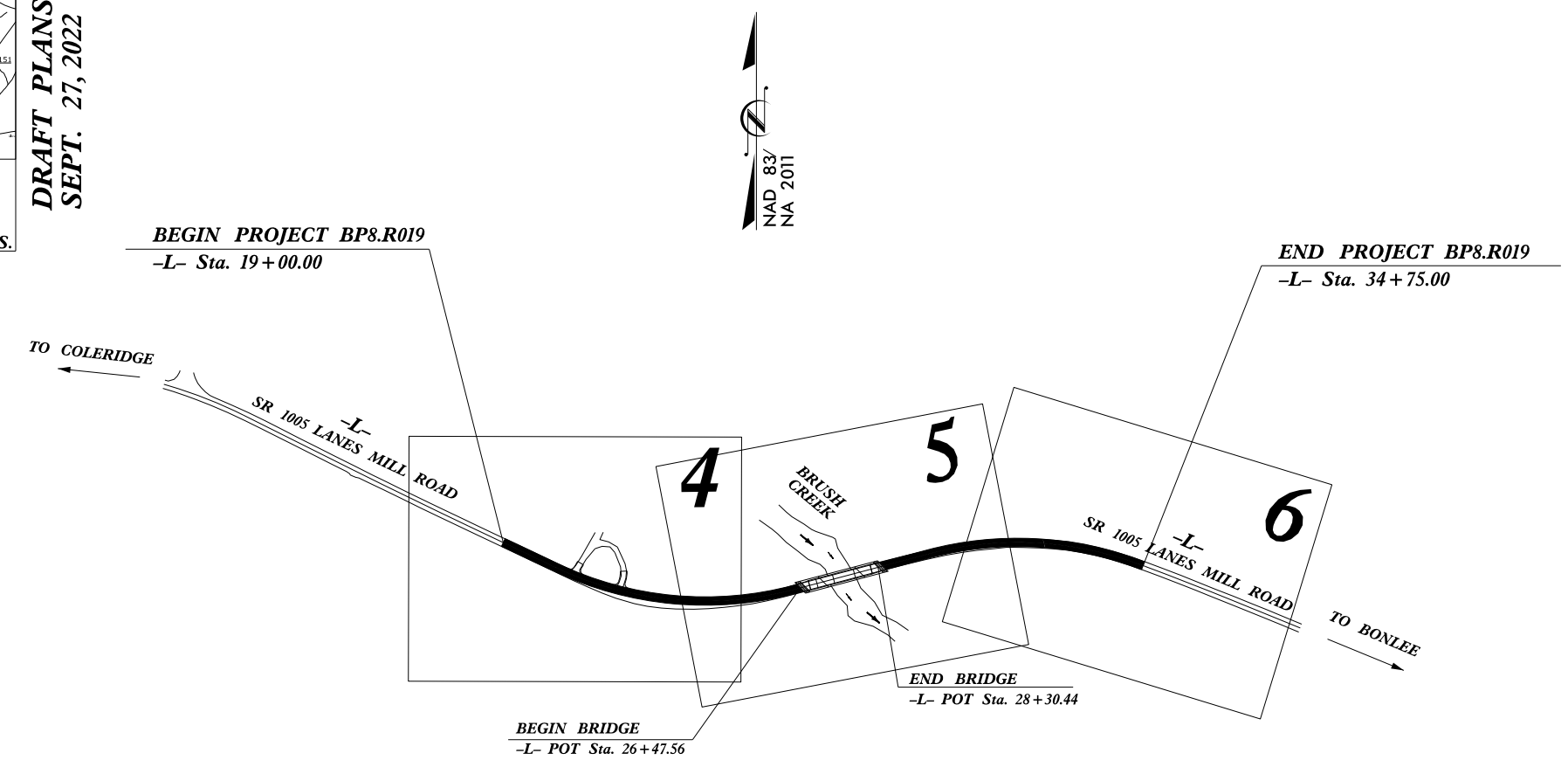
**LOCATION: BRIDGE 750162 OVER BRUSH CREEK
ON SR 1005 (LANES MILL ROAD)**

TYPE OF WORK: GRADING, DRAINAGE, PAVING & STRUCTURES

STATE	STATE PROJECT REFERENCE NO.	SHEET NO.	TOTAL SHEETS
N.C.	BP8.R019	3	
STATE PROJ. NO.	F.A. PROJ. NO.	DESCRIPTION	
BP8.R019.1		P.E.	
		R/W & Utilities	
		Construction	



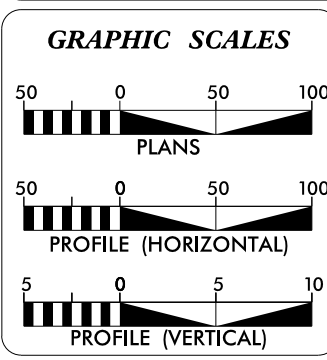
**DRAFT PLANS
SEPT. 27, 2022**



CLEARING ON THIS PROJECT SHALL BE PERFORMED TO LIMITS ESTABLISHED BY METHOD III.

INCOMPLETE PLANS
DO NOT USE FOR R/W ACQUISITION

DOCUMENT NOT CONSIDERED FINAL
UNLESS ALL SIGNATURES COMPLETED



DESIGN DATA

ADT 2016	=	430
ADT 2040	=	860
K	=	%
D	=	%
T	=	6 % *
V	=	50 MPH
* TTST	=	DUAL
FUNC CLASS	=	
LOCAL	=	
SUBREGIONAL TIER	=	

PROJECT LENGTH

LENGTH ROADWAY PROJECT BP8.R019	=	0.263 mi
LENGTH STRUCTURE PROJECT BP8.R019	=	0.035 mi
TOTAL LENGTH OF PROJECT BP8.R019	=	0.298 mi

PLANS PREPARED BY:
CH ENGINEERING
3220 GLEN ROYAL RD. RALEIGH, NC 27617
TEL: 919.788.9224 FAX: 919.788.0292
NC LICENSE #P-0189

2018 STANDARD SPECIFICATIONS

RIGHT OF WAY DATE:
NOVEMBER 10, 2022

LETTING DATE:
OCTOBER 22, 2024

PLANS PREPARED FOR:
DIVISION OF HIGHWAYS
DIVISION 8
121 DOT Drive
Carthage, NC 28327

BRIAN A. WILES, PE
PROJECT ENGINEER

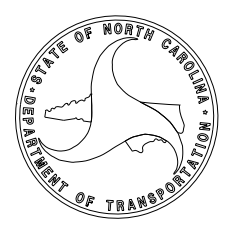
TIM WELCH, PE
NCDOT CONTACT
DIV 8 BRIDGE PROGRAM MANAGER

HYDRAULICS ENGINEER
M.E. ENGINEERING

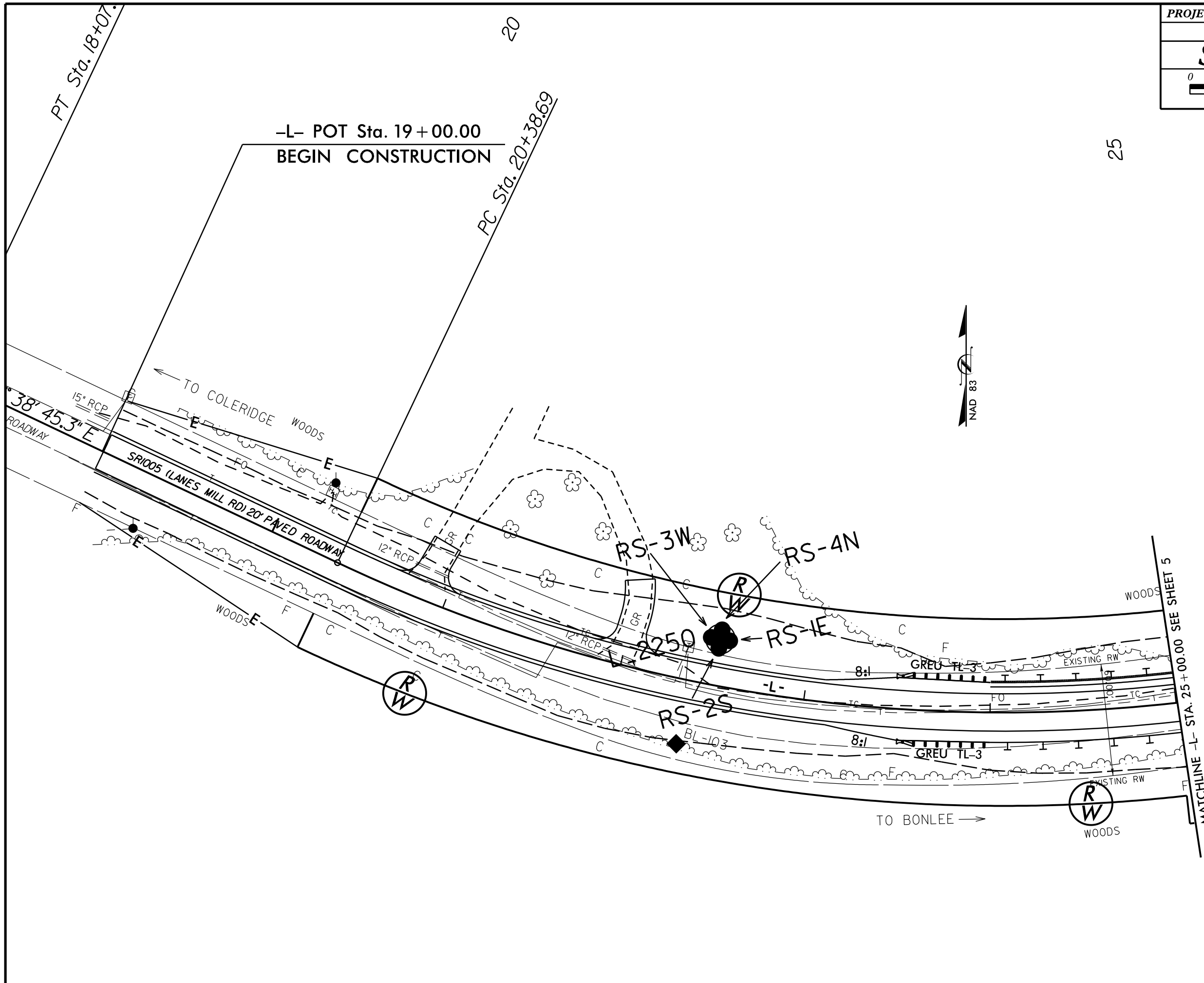
SIGNATURE: _____ P.E.

ROADWAY DESIGN ENGINEER

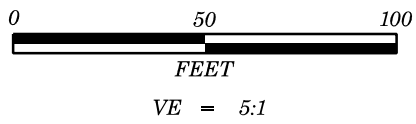
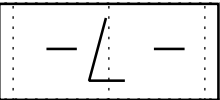
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\$\$\$\$\$ SYSTEM \$\$\$\$\$\$ DGN \$\$\$\$\$\$ USERNAME \$\$\$\$\$\$



5/14/99

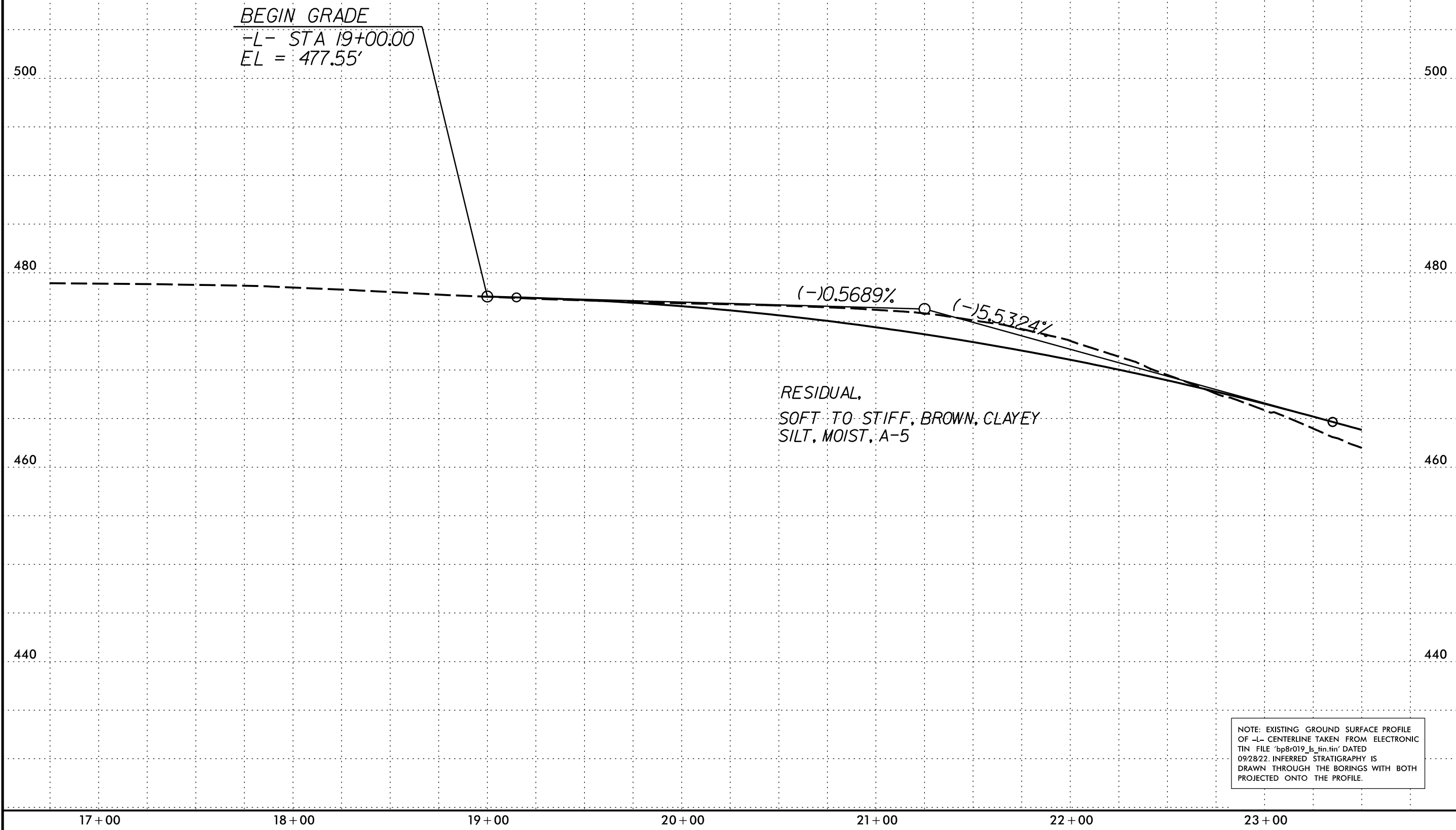


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BP8.R019

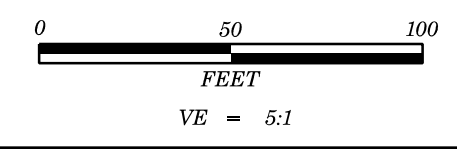
7

PROFILE PROJECTED ALONG CENTERLINE OF -L-



NOTE: EXISTING GROUND SURFACE PROFILE OF -L- CENTERLINE TAKEN FROM ELECTRONIC TIN FILE 'bp8r019_ls_fin.tin' DATED 09/28/22. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE PROFILE.

5/14/99



PROJECT REFERENCE NO.	SHEET NO.
BP8.R019	8
PROFILE PROJECTED ALONG CENTERLINE OF -L-	

- (A) ROADWAY EMBANKMENT, STIFF TO VERY STIFF, BROWN, SILTY CLAY AND SANDY CLAY, MOIST, A-7-5 & A-6
- (B) ALLUVIAL, STIFF TO VERY STIFF, BROWN, SILTY CLAY, MOIST, A-7-5
- (C) RESIDUAL, MEDIUM STIFF TO HARD, BROWN, SANDY SILT AND CLAYEY SILT, MOIST, A-4 & A-5
- (D) ROADWAY EMBANKMENT, MEDIUM STIFF TO VERY STIFF, BROWN, SANDY SILT, CLAYEY SILT AND LOOSE, SILTY SAND, TRACE GRAVEL, MOIST, A-4, A-5 & A-2-4
- (E) RESIDUAL, STIFF, BROWN, CLAY, MOIST, A-7-6

EB1-B
26+53
7' RT
-L-
SS-15

EB2-B
28+33
7' RT
-L-

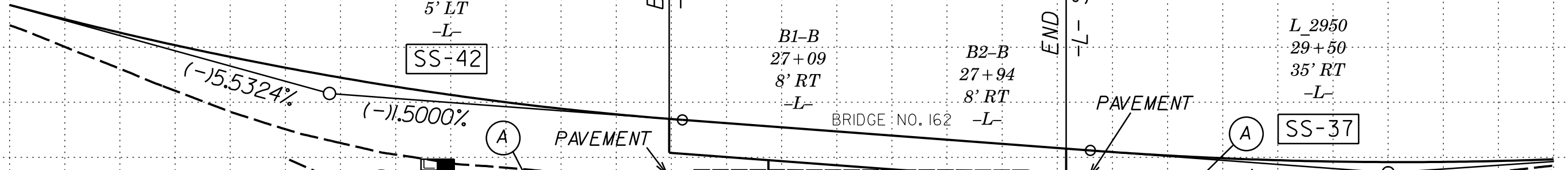
(F) WEATHERED ROCK, META-ARGILLITE

480

480

460

460



L 2550
25+50
5' LT
-L-
SS-42

B1-B
27+09
8' RT
-L-

B2-B
27+94
8' RT
-L-

L 2950
29+50
35' RT
-L-

SS-37

RESIDUAL, STIFF TO VERY STIFF, BROWN, SANDY CLAY, MOIST, A-6

WEATHERED ROCK, META-ARGILLITE

NON-CRYSTALLINE ROCK, GRAY, MODERATE WEATHERING TO FRESH, VERY CLOSE TO WIDE FRACTURE SPACING, HARD, INDURATED, THICKLY BEDDED, META-ARGILLITE

REC. = 99%
RQD = 79%
GSI = 70-80

REC. = 99%
RQD = 82%
GSI = 70-80

440

440

420

420

400

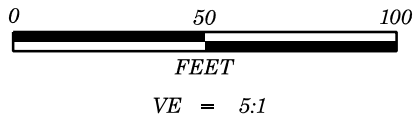
400

24+00 25+00 26+00 27+00 28+00 29+00 30+00

NOTE: EXISTING GROUND SURFACE PROFILE OF -L- CENTERLINE TAKEN FROM ELECTRONIC TIN FILE 'bp8r019_ls_fin.tin' DATED 09/28/22. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE PROFILE.

5/14/99

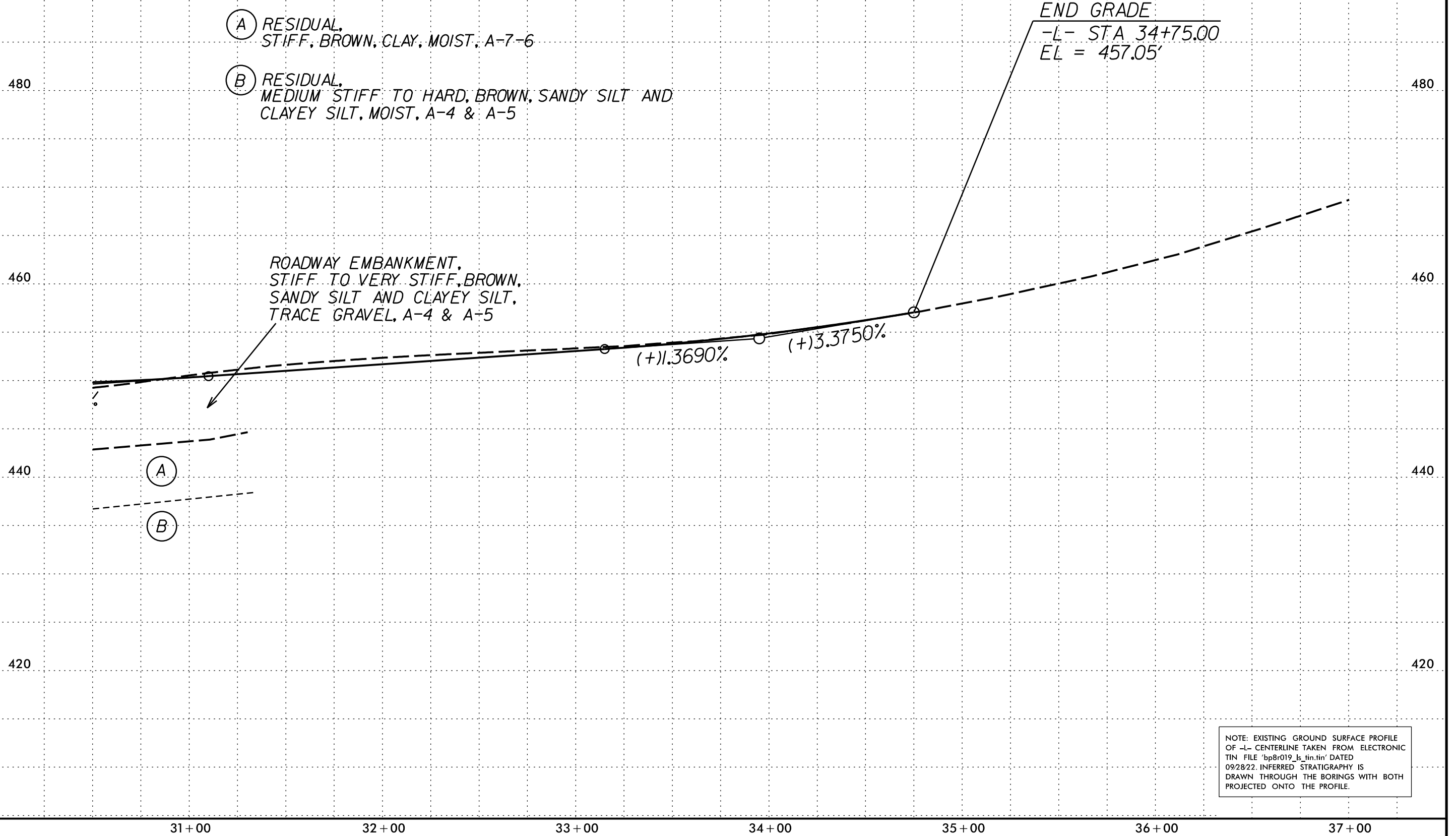
-L-



PROJECT REFERENCE NO. SHEET NO.

BP8.R019 9

PROFILE PROJECTED ALONG CENTERLINE OF -L-



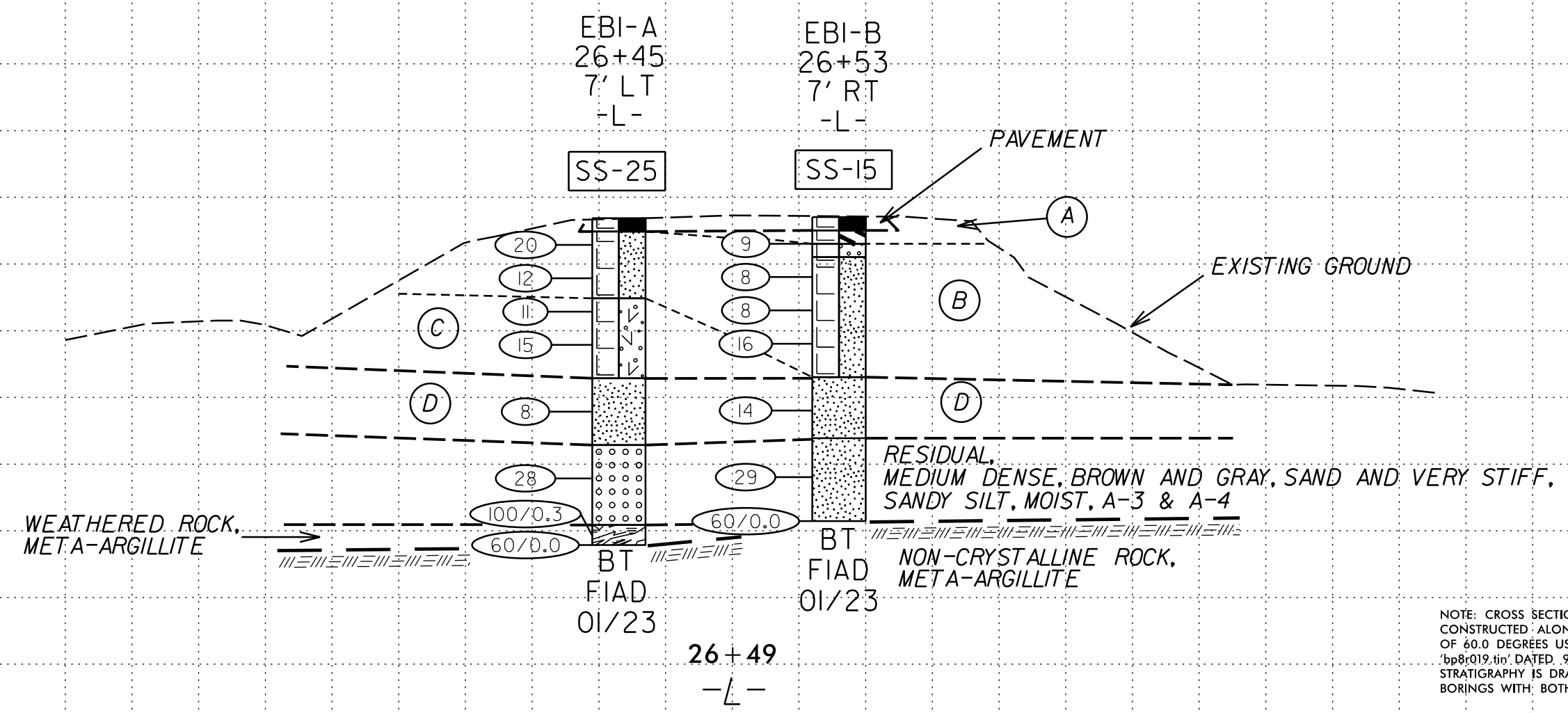
NOTE: EXISTING GROUND SURFACE PROFILE OF -L- CENTERLINE TAKEN FROM ELECTRONIC TIN FILE 'bp8r019_ls_fin.tin' DATED 09/28/22. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO THE PROFILE.

6/23/16
SECTION
NO.
DATE
DRAWN
BY

BRIDGE NO. 162

- (A) ROADWAY EMBANKMENT, STIFF, BROWN, SILTY CLAY, WET, A-7-5
- (B) ROADWAY EMBANKMENT, STIFF TO VERY STIFF, BROWN, SANDY SILT, AND LOOSE, SILTY SAND, TRACE GRAVEL, MOIST, A-4 & A-2-4
- (C) ROADWAY EMBANKMENT, STIFF, BROWN, CLAYEY SILT, TRACE GRAVEL, MOIST, A-5
- (D) ALLUVIAL, STIFF, BROWN, SANDY SILT, TRACE ORGANIC MATTER, MOIST, A-4

CROSS SECTION ALONG END BENT I

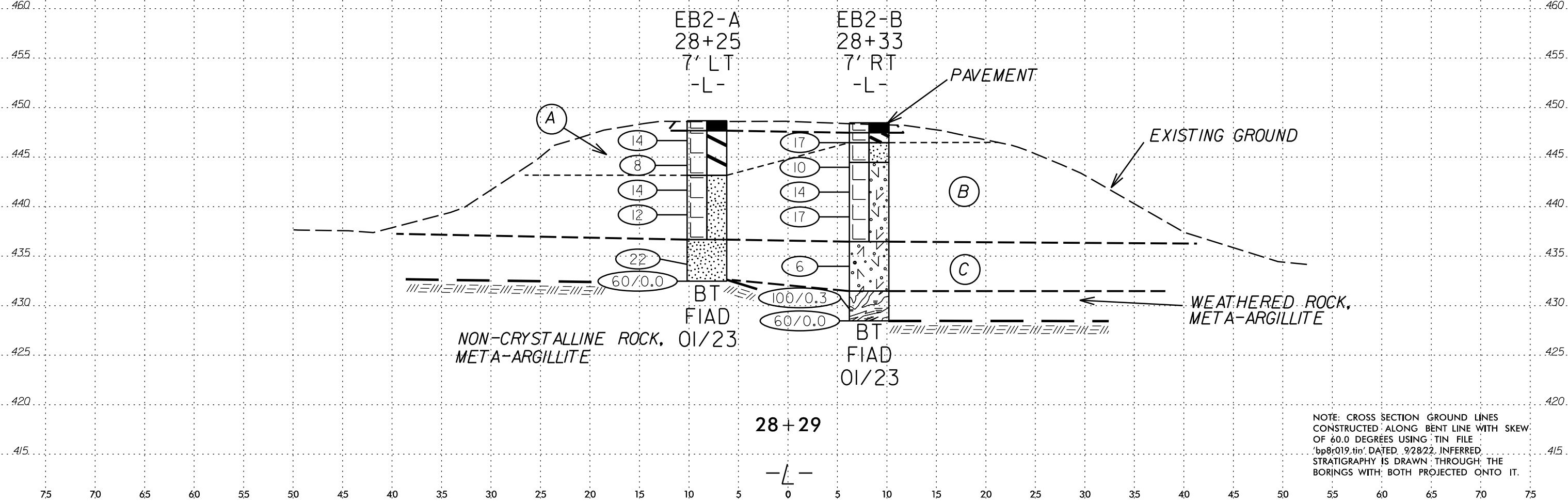


NOTE: CROSS SECTION GROUND LINES CONSTRUCTED ALONG BENT LINE WITH SKEW OF 60.0 DEGREES USING TIN FILE 'bp8r019.tin' DATED 9/28/22. INFERRED STRATIGRAPHY IS DRAWN THROUGH THE BORINGS WITH BOTH PROJECTED ONTO IT.

BRIDGE NO. 162

- (A) ROADWAY EMBANKMENT, STIFF, BROWN, SILTY CLAY, MOIST, A-7-5
- (B) ROADWAY EMBANKMENT, STIFF TO VERY STIFF, BROWN, SANDY SILT AND CLAYEY SILT, MOIST, A-4 & A-5
- (C) RESIDUAL, MEDIUM STIFF TO VERY STIFF, BROWN, SANDY SILT AND CLAYEY SILT, MOIST, A-4 & A-5

CROSS SECTION ALONG END BENT 2



NOTE: CROSS SECTION GROUND LINES
CONSTRUCTED ALONG BENT LINE WITH SKEW
OF 60.0 DEGREES USING TIN FILE
'bp8r019.tin' DATED 9/28/22. INFERRED
STRATIGRAPHY IS DRAWN THROUGH THE
BORINGS WITH BOTH PROJECTED ONTO IT.

GEOTECHNICAL BORING REPORT

BORE LOG

WBS N/A		TIP BP8.R019		COUNTY RANDOLPH		GEOLOGIST Melecosky, S.										
SITE DESCRIPTION BRIDGE NO. 162 ON SR 1005 (-L-) OVER BRUSH CREEK							GROUND WTR (ft)									
BORING NO. EB1-A		STATION 26+45		OFFSET 7 ft LT		ALIGNMENT -L-										
COLLAR ELEV. 448.4 ft		TOTAL DEPTH 24.5 ft		NORTHING 688,891		EASTING 1,828,711										
DRILL RIG/HAMMER EFF./DATE SVE383 DIEDRICH D-50 88% 08/22/2022			DRILL METHOD H.S. Augers			HAMMER TYPE Automatic										
DRILLER Williams, T.		START DATE 01/23/23		COMP. DATE 01/23/23		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)		
			0.5ft	0.5ft	0.5ft	0	25	50	75	100						
450																
	447.4	1.0	16	10	10										448.4	0.0
	447.4	1.0													447.4	1.0
445	444.9	3.5	3	5	7											
	442.4	6.0	4	5	6										442.4	6.0
440	439.9	8.5	8	7	8											
	434.9	13.5	2	3	5										436.4	12.0
435	434.9	13.5														
	429.9	18.5	7	12	16										431.4	17.0
430	429.9	18.5														
	424.9	23.5													425.4	23.0
	423.9	24.5	100/0.3												423.9	24.5
		60/0.0														

WBS N/A		TIP BP8.R019		COUNTY RANDOLPH		GEOLOGIST Melecosky, S.										
SITE DESCRIPTION BRIDGE NO. 162 ON SR 1005 (-L-) OVER BRUSH CREEK							GROUND WTR (ft)									
BORING NO. EB1-B		STATION 26+53		OFFSET 7 ft RT		ALIGNMENT -L-										
COLLAR ELEV. 448.5 ft		TOTAL DEPTH 22.8 ft		NORTHING 688,879		EASTING 1,828,723										
DRILL RIG/HAMMER EFF./DATE SVE383 DIEDRICH D-50 88% 08/22/2022			DRILL METHOD H.S. Augers			HAMMER TYPE Automatic										
DRILLER Williams, T.		START DATE 01/23/23		COMP. DATE 01/23/23		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG	SOIL AND ROCK DESCRIPTION	DEPTH (ft)		
			0.5ft	0.5ft	0.5ft	0	25	50	75	100						
450																
	447.5	1.0	5	4	5										448.5	0.0
	447.5	1.0													447.5	1.0
445	445.0	3.5	3	3	5										446.5	2.0
	442.5	6.0	3	3	5										445.5	3.0
440	440.0	8.5	4	7	9											
	435.0	13.5	5	6	8										436.5	12.0
435	435.0	13.5														
	430.0	18.5	6	13	16										431.5	17.0
430	430.0	18.5														
	425.7	22.8													425.7	22.8
		60/0.0														

NCDOT BORE DOUBLE RANDOLPH BR 162.GPJ NC_DOT_GDT 10/2/23

GEOTECHNICAL BORING REPORT BORE LOG

GEOTECHNICAL BORING REPORT CORE LOG

WBS N/A		TIP BP8.R019		COUNTY RANDOLPH		GEOLOGIST Melecovsky, S.									
SITE DESCRIPTION BRIDGE NO. 162 ON SR 1005 (-L-) OVER BRUSH CREEK							GROUND WTR (ft)								
BORING NO. B1-A		STATION 27+00		OFFSET 8 ft LT		ALIGNMENT -L-									
COLLAR ELEV. 431.5 ft		TOTAL DEPTH 24.9 ft		NORTHING 688,906		EASTING 1,828,764									
DRILL RIGHAMMER EFF./DATE SVE383 DIEDRICH D-50 88% 08/22/2022		DRILL METHOD Mud Rotary		HAMMER TYPE Automatic											
DRILLER Williams, T.		START DATE 01/26/23		COMP. DATE 01/26/23		SURFACE WATER DEPTH N/A									
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	L O G	SOIL AND ROCK DESCRIPTION	DEPTH (ft)	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100					
435															
430	431.5	0.0	WOH	WOH	1							M	GROUND SURFACE	0.0	
425	427.2	4.3	60/0.0										ALLUVIAL VERY SOFT, BROWN, SILTY CLAY, TRACE ORAGANIC MATTER, A-7-6	4.3	
420													WEATHERED ROCK (META-ARGILLITE)	7.5	
415												RS-1	NON-CRYSTALLINE ROCK GRAY, MODERATE WEATHERING TO FRESH, VERY CLOSE TO WIDE FRACTURE SPACING, HARD, INDURATED, THICKLY BEDDED, META-ARGILLITE		
410												RS-2	REC = 100% RQD = 91% GSI = 70-80		
													Boring Terminated at Elevation 406.6 ft IN NON-CRYSTALLINE ROCK (META-ARGILLITE)	24.9	

WBS N/A		TIP BP8.R019		COUNTY RANDOLPH		GEOLOGIST Melecovsky, S.						
SITE DESCRIPTION BRIDGE NO. 162 ON SR 1005 (-L-) OVER BRUSH CREEK							GROUND WTR (ft)					
BORING NO. B1-A		STATION 27+00		OFFSET 8 ft LT		ALIGNMENT -L-						
COLLAR ELEV. 431.5 ft		TOTAL DEPTH 24.9 ft		NORTHING 688,906		EASTING 1,828,764						
DRILL RIGHAMMER EFF./DATE SVE383 DIEDRICH D-50 88% 08/22/2022		DRILL METHOD Mud Rotary		HAMMER TYPE Automatic								
DRILLER Williams, T.		START DATE 01/26/23		COMP. DATE 01/26/23		SURFACE WATER DEPTH N/A						
ELEV (ft)	RUN ELEV (ft)	DEPTH (ft)	RUN (ft)	DRILL RATE (Min/ft)	TOTAL RUN 20.6 ft		SAMP. NO.	STRATA		L O G	DESCRIPTION AND REMARKS	DEPTH (ft)
					REC. (ft) %	RQD (ft) %		REC. (ft) %	RQD (ft) %			
427.18											Begin Coring @ 4.3 ft	
425	427.2	4.3	4.6	N=60/0.0 1:34/0.6 2:40/1.0 2:55/1.0 3:15/1.0 1:46/1.0	(3.0) 65%	(1.1) 24%					WEATHERED ROCK (META-ARGILLITE)	4.3
420	422.6	8.9	5.0	2:07/1.0 2:34/1.0 2:50/1.0 2:50/1.0 3:05/1.0	(5.0) 100%	(4.5) 90%	RS-1	(17.4) 100%	(15.9) 91%		NON-CRYSTALLINE ROCK GRAY, MODERATE WEATHERING TO FRESH, VERY CLOSE TO WIDE FRACTURE SPACING, HARD, INDURATED, THICKLY BEDDED, META-ARGILLITE	7.5
415	417.6	13.9	5.0	2:58/1.0 2:41/1.0 2:48/1.0 2:50/1.0 3:15/1.0	(5.0) 100%	(4.3) 86%	RS-2				GSI = 70-80	
410	412.6	18.9	5.0	2:26/1.0 3:00/1.0 2:52/1.0 2:50/1.0 2:58/1.0	(5.0) 100%	(5.0) 100%						
	407.6	23.9	1.0	2:11/1.0	(1.0) 100%	(1.0) 100%					Boring Terminated at Elevation 406.6 ft IN NON-CRYSTALLINE ROCK (META-ARGILLITE)	24.9

GEOTECHNICAL BORING REPORT

BORE LOG

WBS N/A		TIP BP8.R019		COUNTY RANDOLPH		GEOLOGIST Melecosky, S.										
SITE DESCRIPTION BRIDGE NO. 162 ON SR 1005 (-L-) OVER BRUSH CREEK							GROUND WTR (ft)									
BORING NO. EB2-A		STATION 28+25		OFFSET 7 ft LT		ALIGNMENT -L-										
COLLAR ELEV. 448.7 ft		TOTAL DEPTH 16.2 ft		NORTHING 688,937		EASTING 1,828,885										
DRILL RIG/HAMMER EFF./DATE SVE383 DIEDRICH D-50 88% 08/22/2022		DRILL METHOD H.S. Augers		HAMMER TYPE Automatic												
DRILLER Williams, T.		START DATE 01/23/23		COMP. DATE 01/23/23		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG MOI	LOG G	SOIL AND ROCK DESCRIPTION	DEPTH (ft)	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100						
450																
	447.7	1.0	11	6	8										448.7	0.0
	447.7														447.7	1.0
445	445.2	3.5	3	3	5											
	442.7	6.0	5	7	7											
440	440.2	8.5	4	6	6											
	435.2	13.5	6	10	12											
	432.5	16.2	60/0.0												432.5	16.2
Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 432.5 ft ON NON-CRYSTALLINE ROCK (META-ARGILLITE)																

WBS N/A		TIP BP8.R019		COUNTY RANDOLPH		GEOLOGIST Melecosky, S.										
SITE DESCRIPTION BRIDGE NO. 162 ON SR 1005 (-L-) OVER BRUSH CREEK							GROUND WTR (ft)									
BORING NO. EB2-B		STATION 28+33		OFFSET 7 ft RT		ALIGNMENT -L-										
COLLAR ELEV. 448.5 ft		TOTAL DEPTH 20.0 ft		NORTHING 688,925		EASTING 1,828,897										
DRILL RIG/HAMMER EFF./DATE SVE383 DIEDRICH D-50 88% 08/22/2022		DRILL METHOD H.S. Augers		HAMMER TYPE Automatic												
DRILLER Williams, T.		START DATE 01/23/23		COMP. DATE 01/23/23		SURFACE WATER DEPTH N/A										
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	LOG MOI	LOG G	SOIL AND ROCK DESCRIPTION	DEPTH (ft)	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100						
450																
	447.5	1.0	13	9	8										448.5	0.0
	447.5														447.5	1.0
	446.5														446.5	2.0
445	445.0	3.5	2	5	5										444.5	4.0
	442.5	6.0	5	7	7											
440	440.0	8.5	5	7	10											
	435.0	13.5	3	3	3											
430	430.0	18.5														
	428.5	20.0	100/0.3												431.5	17.0
			60/0.0												428.5	20.0
Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 428.5 ft ON NON-CRYSTALLINE ROCK (META-ARGILLITE)																

NCDOT BORE DOUBLE RANDOLPH BR 162.GPJ NC_DOT_GDT 10/2/23

GEOTECHNICAL BORING REPORT

BORE LOG

WBS N/A		TIP BP8.R019		COUNTY RANDOLPH		GEOLOGIST Melecosky, S.									
SITE DESCRIPTION BRIDGE NO. 162 ON SR 1005 (-L-) OVER BRUSH CREEK							GROUND WTR (ft)								
BORING NO. L_2250		STATION 22+50		OFFSET 25 ft LT		ALIGNMENT -L-									
COLLAR ELEV. 472.5 ft		TOTAL DEPTH 0.7 ft		NORTHING 688,890		EASTING 1,828,327									
DRILL RIGHAMMER EFF./DATE N/A		DRILL METHOD Hand Auger		HAMMER TYPE N/A											
DRILLER Williams, T.		START DATE 02/07/23		COMP. DATE 02/07/23		SURFACE WATER DEPTH N/A									
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100					ELEV. (ft)
475															
															GROUND SURFACE 472.5 RESIDUAL 471.8 SOFT TO STIFF, TAN, CLAYEY SILT, A-5 Boring Terminated at Elevation 471.8 ft ON WEATHERED ROCK (META-ARGILLITE) Hand Auger refusal at 0.7 feet.

WBS N/A		TIP BP8.R019		COUNTY RANDOLPH		GEOLOGIST Melecosky, S.									
SITE DESCRIPTION BRIDGE NO. 162 ON SR 1005 (-L-) OVER BRUSH CREEK							GROUND WTR (ft)								
BORING NO. L_2550		STATION 25+50		OFFSET 5 ft LT		ALIGNMENT -L-									
COLLAR ELEV. 449.8 ft		TOTAL DEPTH 17.1 ft		NORTHING 688,868		EASTING 1,828,620									
DRILL RIGHAMMER EFF./DATE SME383 DIEDRICH D-50 88% 08/22/2022		DRILL METHOD H.S. Augers		HAMMER TYPE Automatic											
DRILLER Williams, T.		START DATE 01/27/23		COMP. DATE 01/27/23		SURFACE WATER DEPTH N/A									
ELEV (ft)	DRIVE ELEV (ft)	DEPTH (ft)	BLOW COUNT			BLOWS PER FOOT					SAMP. NO.	MOI	LOG	SOIL AND ROCK DESCRIPTION	
			0.5ft	0.5ft	0.5ft	0	25	50	75	100					ELEV. (ft)
450															
	448.8	1.0	11	8	8										GROUND SURFACE 449.8 ROADWAY EMBANKMENT (PAVEMENT) 448.8 VERY STIFF, BROWN, SANDY CLAY, TRACE GRAVEL, A-6 445.8 RESIDUAL VERY STIFF TO HARD, TAN, SANDY CLAY, A-6 WEATHERED ROCK (META-ARGILLITE) 437.8 Boring Terminated WITH STANDARD PENETRATION TEST REFUSAL at Elevation 432.7 ft ON NON-CRYSTALLINE ROCK (META-ARGILLITE) 432.7
	446.3	3.5	4	6	13										
	443.8	6.0	11	16	23										
	441.3	8.5	9	10	11										
	436.3	13.5	100/0.4												
	432.7	17.1	60/0.0												

NCDOT BORE DOUBLE RANDOLPH BR 162.GPJ NC_DOT_GDT 10/2/23

FORM NO. TR-43-D7012C-
02
Revision No. : 0
Revision Date: 08/22/18

UNCONFINED COMPRESSION (ASTM D7012 Method C)



S&ME, Inc. - Knoxville 1413 Topside Road, Louisville, TN 37777

Project Name: Bridge No. 162
Project Number: 213636A

Report Date: June 16, 2023
Reviewed By: JD

Boring No.	Sample No.	Depth (ft)	Dimensions, in.		Shape (See Key)	Area (in ²)	Unit Weight (lbs/ft ³)	Loading Rate (psi/sec)	Maximum Load (lbs)	Strength (psi)	Moisture (%)	Time to Failure (s)
			Length	Diameter								
B1-A	RS-1	8.95 - 9.35	4.52	1.86	A	2.72	177.1	81	30,296	11,138	0.1	137.5
B1-A	RS-2	11.00 - 11.40	4.30	1.86	A	2.72	174.8	103	57,898	21,286	0.1	206.7
B1-B	RS-3	12.75 - 13.15	4.32	1.86	A	2.72	175.8	106	61,139	22,478	0.0	212.1
B2-B	RS-4	8.35 - 8.75	4.36	1.86	A	2.72	174.7	80	22,936	8,432	0.1	105.4
B2-B	RS-5	11.35 - 11.75	4.33	1.86	A	2.72	175.2	99	53,065	19,509	0.0	197.1

NOTES: Effective (as received) unit weight as determined by RTH 109-93.

Loading rates were selected to target reaching failure between 2 and 15 minutes.

Test results for specimens not meeting the requirements of ASTM D4543-19 may differ from a test specimen that meets the requirements of ASTM D4543.

SHAPE KEY

ASTM D4543-19 Standard Practice for Preparing Rock Core as Cylindrical Test Specimens and Verifying Conformance to Dimensional and Shape Tolerance Section 1.2 - "Rock is a complex engineering material that can vary greatly as a function of lithology, stress history, weathering, moisture content and chemistry, and other natural geologic processes. As such, it is not always possible to obtain or prepare rock core specimens that satisfy the desirable tolerances given in this practice. Most commonly, this situation presents itself with weaker, more porous, and poorly cemented rock types and rock types containing significant or weak (or both) structural features. For rock types which are difficult to prepare, all reasonable efforts shall be made to prepare a specimen in accordance with this practice and for the intended test procedure. However, when it has been determined by trial and error that this is not possible, prepare the rock specimen to the closest tolerances practicable and consider this to be the best effort and report it as such and if allowable or necessary for the intended test, capping the ends of the specimen as discussed in this practice is permitted."

- A Test specimen measurements met the desired shape tolerances of ASTM D4543-19 (side straightness, end flatness & parallelism, and end perpendicularity to axis)
- B Test specimen measurements met the desired shape tolerances of ASTM D4543-19 for end flatness & parallelism, and end perpendicularity to axis. Specimen did not meet the desired tolerance for side straightness. Specimen prepared to closest tolerances practicable.
- C Test specimen measurements met the desired shape tolerances of ASTM D4543-19 for end flatness & parallelism. Specimen did not meet the desired tolerances for side straightness and end perpendicularity to axis. Specimen prepared to closest tolerances practicable.
- D Test specimen measurements met the desired shape tolerances of ASTM D4543-19 for end flatness. Specimen did not meet the desired tolerances for side straightness, parallelism and end perpendicularity to axis. Specimen prepared to closest tolerances practicable.
- E Test specimen measurements met the desired shape tolerances of ASTM D4543-19 for end flatness and end perpendicularity to axis. Specimen did not meet the desired tolerance for side straightness and parallelism. Specimen prepared to closest tolerances practicable.

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1	Location / Orientation	B1-A, RS-1 (9.0' – 9.4')	Photographer: Ryan Skinner Date: 06/16/2023
	Remarks	Unconfined Compressive Strength of Rock Core Specimen B1-Before/After (ASTM D7012 Method C)	

2	Location / Orientation	B1-A, RS-2 (11.00' – 11.40')	Photographer: Ryan Skinner Date: 06/16/2023
	Remarks	Unconfined Compressive Strength of Rock Core Specimen B1-Before/After (ASTM D7012 Method C)	

3	Location / Orientation	B1-B, RS-3 (12.8' – 13.2')	Photographer: Ryan Skinner Date: 06/16/2023
	Remarks	Unconfined Compressive Strength of Rock Core Specimen B1-Before/After (ASTM D7012 Method C)	

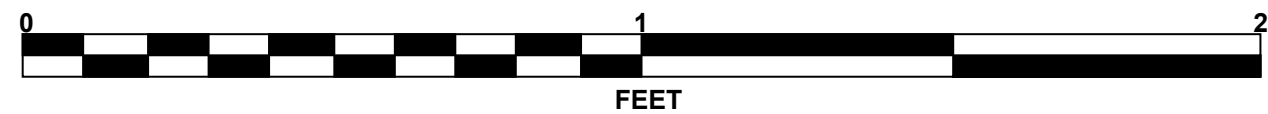
4	Location / Orientation	B2-B, RS-4 (8.4' – 8.8')	Photographer: Ryan Skinner Date: 06/16/2023
	Remarks	Unconfined Compressive Strength of Rock Core Specimen B1-Before/After (ASTM D7012 Method C)	

		Date: 06/16/2023
		Photographer: Ryan Skinner
5	Location / Orientation	B2-B, RS-5 (11.4' – 11.8')
	Remarks	Unconfined Compressive Strength of Rock Core Specimen B1-Before/After (ASTM D7012 Method C)

CORE PHOTOGRAPHS

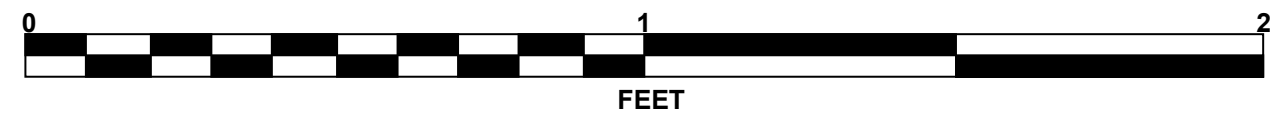
B1-A

BOXES 1 & 2: 4.3 - 18.9 FEET



B1-A

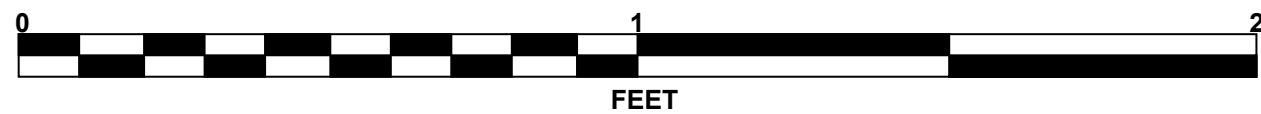
BOX 3: 18.9 - 24.9 FEET



CORE PHOTOGRAPHS

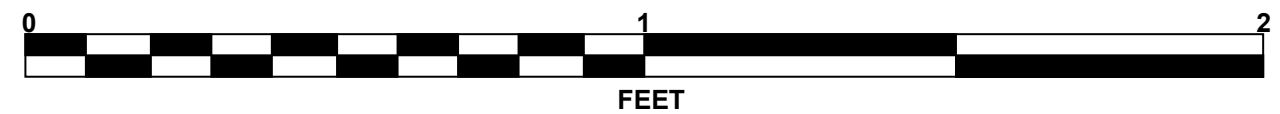
B1-B

BOXES 1 & 2: 6.0 - 22.6 FEET



B1-B

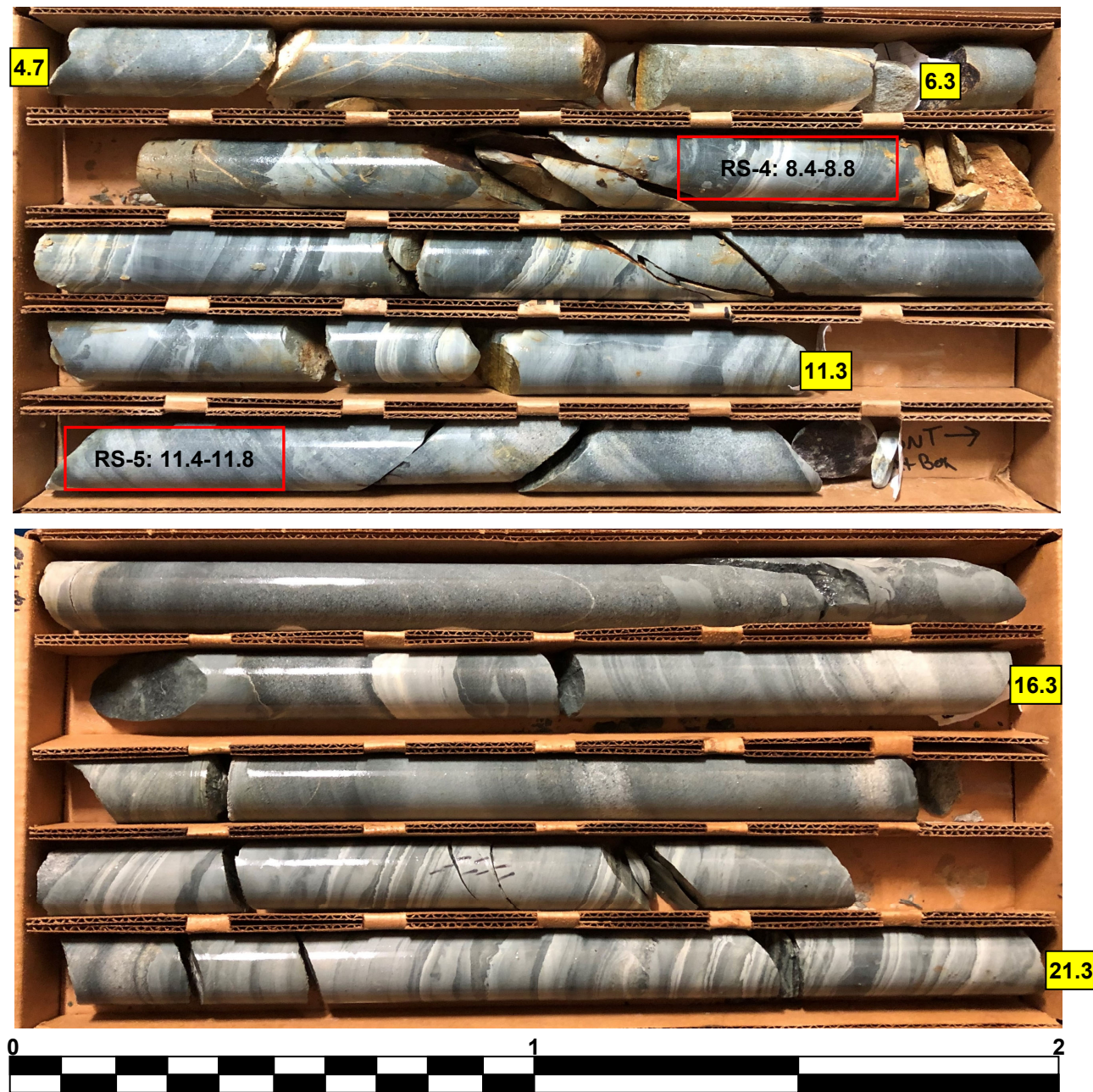
BOX 3: 22.6 - 27.6 FEET



CORE PHOTOGRAPHS

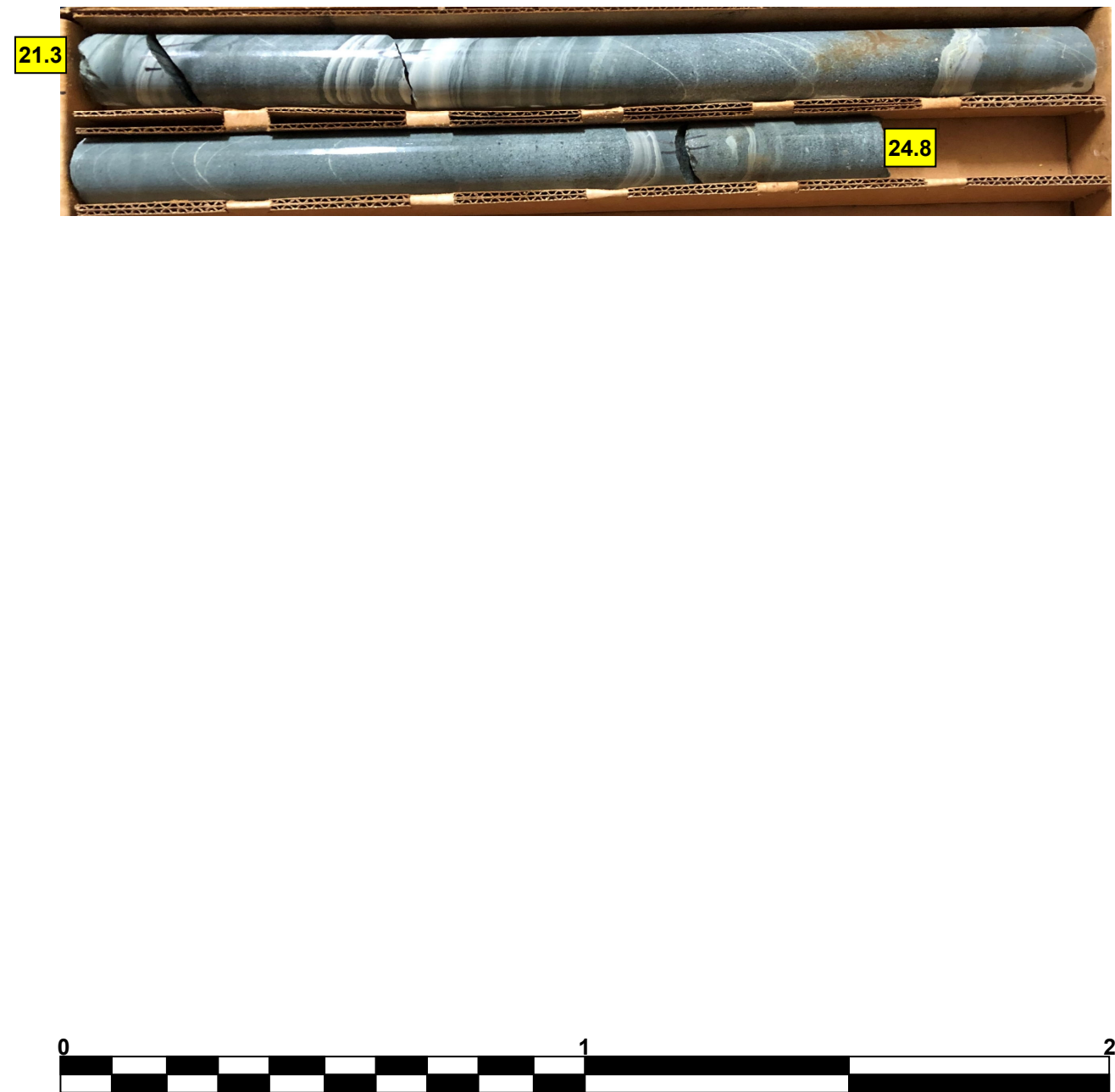
B2-B

BOXES 1 & 2: 4.7 - 21.3 FEET



B2-B

BOX 3: 21.3 - 24.8 FEET



SITE PHOTOGRAPHS

Bridge No. 162 on -L- (SR 1005) over Brush Creek



Looking West